

The sintering behavior and microwave dielectric properties of $\text{Mg}_4(\text{Nb,Sb})_2\text{O}_9$ ceramics

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Abstract The sintering behavior, microstructure and microwave dielectric properties of $\text{Mg}_4(\text{Nb}_{2-x}\text{Sb}_x)\text{O}_9$ ($0 \leq x \leq 2$) solid solutions were investigated systematically by X-ray diffraction (XRD), scanning electron microscopy (SEM) and a network analyzer. The solid solutions of $\text{Mg}_4(\text{Nb}_{2-x}\text{Sb}_x)\text{O}_9$ was formed with x value being no more than 1.6. The dielectric constant (ϵ) of the sintered ceramics decreased from 13.06 to 6.28 with Sb content x from 0 to 1.6. With a substitution of Sb^{5+} for Nb^{5+} ($0.04 \leq x \leq 0.08$), the sintering temperature of $\text{Mg}_4\text{Nb}_2\text{O}_9$ ceramics was decreased from 1400 to 1300 °C without degradation of the Qf values. The optimum microwave dielectric properties of $\epsilon \sim 12.26$, $Qf \sim 168,450$ GHz, and $\tau_f \sim -56.4$ ppm/°C were obtained in the composition of $\text{Mg}_4(\text{Nb}_{1.6}\text{Sb}_{0.4})\text{O}_9$ sintered at 1300 °C.

Keywords Microwave dielectric ceramic · $\text{Mg}_4(\text{Nb}_{2-x}\text{Sb}_x)\text{O}_9$ · High Q · Low ϵ value · Magnesium niobate

1 Introduction

The development of high Q materials with a variety of dielectric constant, ϵ , is essential in the advancement of wireless communication industry. Thus, a number of these materials have been investigated and developed [1–5]. Among which, $\alpha\text{-Al}_2\text{O}_3$ ceramics with corundum structure has a very high Q value ($Qf \sim 300,000$ GHz) and low dielectric constant ($\epsilon \sim 10$), widely used as substrate and IC packaging materials. Very recently, it was found that

$\text{Mg}_4\text{Nb}_2\text{O}_9$ (MN) ceramics exhibited a very high Qf value comparable to Al_2O_3 [6]. By a substitution of Ta^{5+} for Nb^{5+} , the Qf value of $\text{Mg}_4\text{Nb}_2\text{O}_9$ could be further improved [6]. Thus, $\text{Mg}_4\text{Nb}_2\text{O}_9$ is a suitable material for microwave applications, such as substrates and resonators at high frequency. In this work, $\text{Mg}_4(\text{Nb}_{2-x}\text{Sb}_x)\text{O}_9$ ($0 \leq x \leq 2$) solid solutions were fabricated by a conventional solid reaction method and the sintering behavior, microstructures, and microwave dielectric properties of $\text{Mg}_4(\text{Nb}_{2-x}\text{Sb}_x)\text{O}_9$ ceramics were investigated.

2 Experiment procedure

Samples of $\text{Mg}_4(\text{Nb}_{2-x}\text{Sb}_x)\text{O}_9$ ($0 \leq x \leq 2$) were prepared by standard electronic ceramic method. The starting materials were oxide powders: high purity MgO ($\geq 99.9\%$), Nb_2O_5 ($\geq 99.5\%$) and analysis grade Sb_2O_5 ($\leq 99.0\%$). The powders were weighed according to the stoichiometric ratio and then milled in a polyethylene bottle with agate balls for 10 h using alcohol as a medium. Mixtures were dried and calcined at 1000 °C for 10 h. The calcined powders were re-milled for 10 h, then ground with PVA solution as a binder and sieved through a 60-mesh screen. Pellets with 15 mm in diameter and 7 mm in thickness were pressed using uniaxial pressing. These pellets were subsequently sintered at 1300–1400 °C for 5 h in air.

The crystalline phases were analysed by X-ray powder diffraction (XRPD, Rigaku D/max 2550, Japan) using $\text{Cu K}\alpha$ radiation (at 40 Kv and 200 mA) of 2θ from 10° to 80°. The surface microstructure of the as-sintered ceramics were observed by a scanning electron microscopy (Quanta 200 SEM, Holland). The bulk density (ρ) of the sintered pellets was measured by the Archimedes method. The theoretical density (ρ_x) of the ceramics was obtained by using the unit

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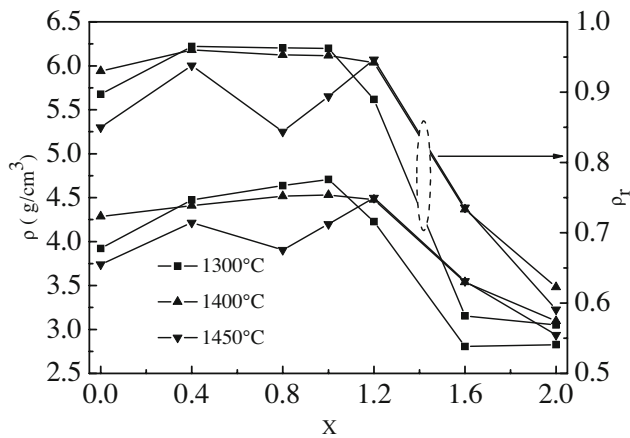


Fig. 1 Bulk density (ρ) and relative density (ρ_r) of $\text{Mg}_4(\text{Nb}_{2-x}\text{Sb}_x)\text{O}_9$ ceramics sintered at different temperatures for 5 h

cell dimensions from the XRPD data. The measurement of dielectric constant (ϵ) and unloaded Q of $\text{Mg}_4\text{Nb}_2\text{O}_9$ ceramics was performed in T_{011} mode at 8–11 GHz by the Hakki-Coleman dielectric resonator method [7] using a network analyzer (Agilent Tech., hp8720ES). The temperature coefficient of resonator frequency (τ_f) was calculated in the temperature between 20–80 °C.

3 Results and discussion

The bulk density (ρ) and relative density (ρ_r) of $\text{Mg}_4(\text{Nb}_{2-x}\text{Sb}_x)\text{O}_9$ ceramics sintered at various temperatures as a function of x values are shown in Fig. 1. At the sintering temperature of 1300 °C, relative density ρ_r increased from 0.87 to 0.96 as x values from 0 to 0.4, and then, ρ_r values saturated at $0.4 \leq x \leq 1.0$. As $x > 1.2$, ρ_r decreased abruptly to 0.57 for $x = 1.6$. This demonstrated that Sb^{5+} substitutions for Nb^{5+} is effective in reducing the sintering temperature of $\text{Mg}_4(\text{Nb}_{2-x}\text{Sb}_x)\text{O}_9$ for $0.4 \leq x \leq 1$, but suppressed the densification process as the

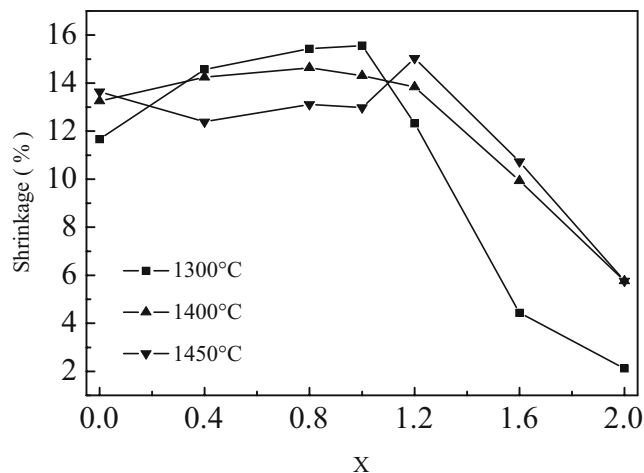


Fig. 2 The shrinkage of $\text{Mg}_4(\text{Nb}_{2-x}\text{Sb}_x)\text{O}_9$ ceramics sintered at different temperatures for 5 h

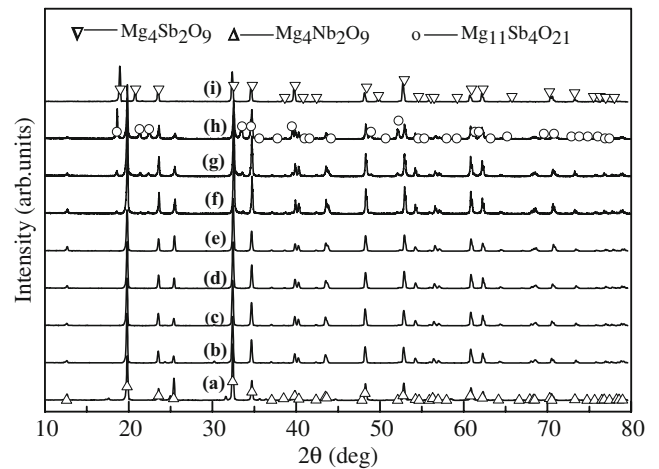


Fig. 3 XRPD patterns of sintered $\text{Mg}_4(\text{Nb}_{2-x}\text{Sb}_x)\text{O}_9$ ceramics (a) $x = 0.4$, (b) $x = 0.8$, (c) $x = 1.0$, (d) $x = 1.2$, (e) $x = 1.6$, (f) $x = 1.7$, (g) $x = 1.8$, (h) $x = 1.9$, (i) $x = 2.0$

compositions $x > 1.2$. The present result is also confirmed by the radical shrinkage(s) of $\text{Mg}_4(\text{Nb}_{2-x}\text{Sb}_x)\text{O}_9$ ceramics sintered at various temperatures as a function x shown in Fig. 2.

Figure 3 shows the XRPD patterns of $\text{Mg}_4(\text{Nb}_{2-x}\text{Sb}_x)\text{O}_9$ with $0 \leq x \leq 2$. The formation of impurity phase was not detected in compositions with $x \leq 1.6$, and the compounds exhibited the ordered corundum structure of $\text{Mg}_4\text{Nb}_2\text{O}_9$ (JCPDS number: 36-1381) with the space group of $P\bar{3}c1$ (No. 165). As the composition x ranged from 1.7 to 1.9, two phases, i.e. $\text{Mg}_4\text{Nb}_2\text{O}_9$ and $\text{Mg}_{11}\text{Sb}_4\text{O}_{21}$ (JCPDS: 23-0380) were found to be co-exist, as shown in Fig. 3(f), (g), and (h), respectively. As $x = 2.0$, the XRPD patterns were indexed as a $\text{Mg}_4\text{Sb}_2\text{O}_9$ phase with the JCPDS number of 23-0378. The lattice parameters, a , c and V , shown in Fig. 4, decreased linearly as the composition x increasing from 0 to 1.6, and

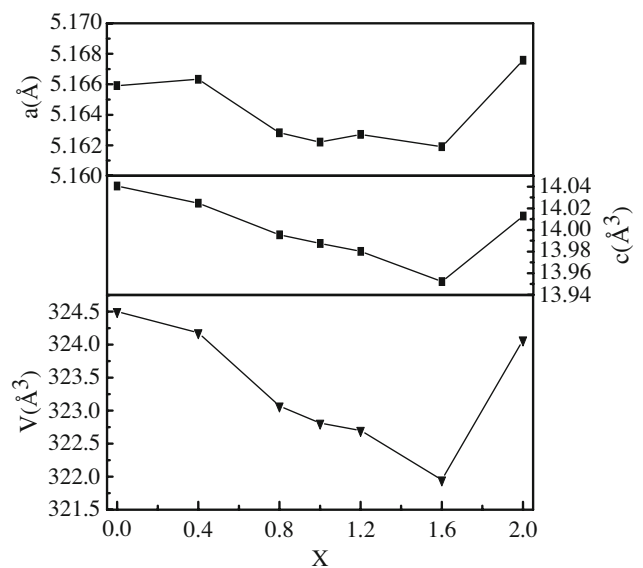


Fig. 4 Lattice parameters, a , c , and unit cell volume V of $\text{Mg}_4(\text{Nb}_{2-x}\text{Sb}_x)\text{O}_9$ ceramics

Fig. 5 SEM micrographs of $Mg_4(Nb_{2-x}Sb_x)O_9$ ceramics sintered at 1300 °C for 5 h: (a) $x=0.0$, (b) $x=0.8$, (c) $x=2.0$, (d) $x=0.8$ sintered at 1450 °C for 5 h

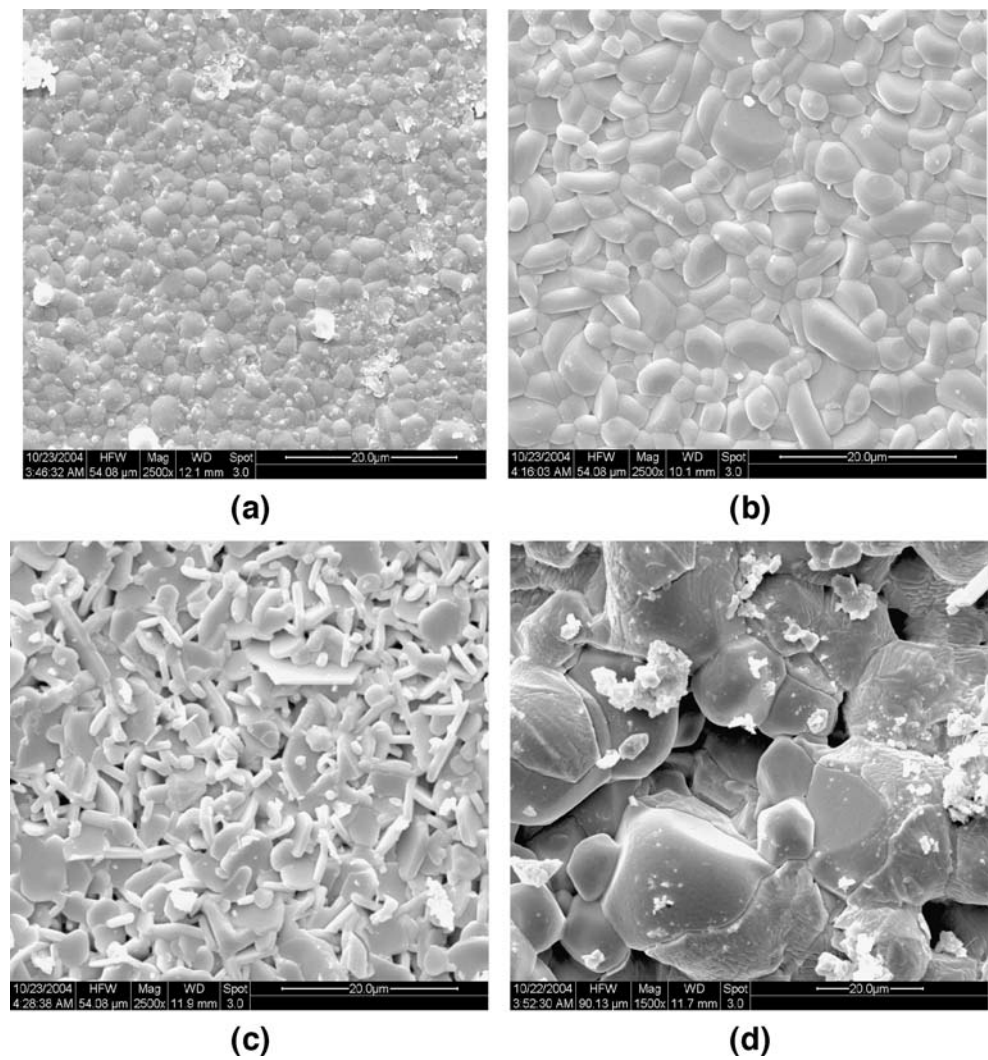


Fig. 6 The dielectric constant, ϵ (a), quality factor, $Q \cdot f$ (b), of $Mg_4(Nb_{2-x}Sb_x)O_9$ ceramics sintered at different temperatures

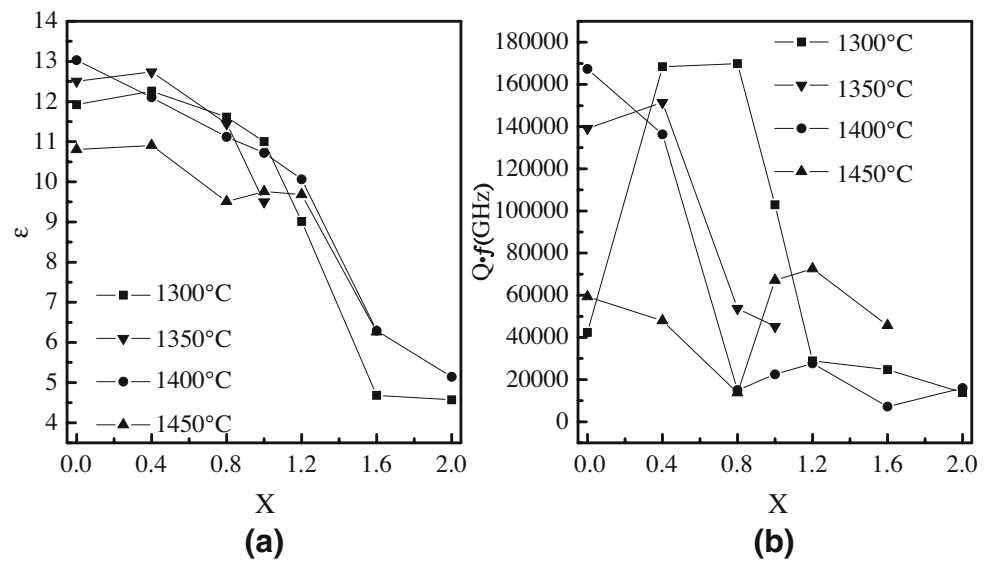


Table 1 The microwave dielectric properties of $\text{Mg}_4(\text{Nb}_{2-x}\text{Sb}_x)\text{O}_9$ ceramics sintered at appropriate temperatures.

Composition x	Sintering temperature (°C)	ρ_r (%)	ϵ	Qf (GHz)	τ_f (ppm/°C)
0	1400	94.4	13.06	162,350	-70.8
0.4	1300	96.0	12.26	168,450	-56.4
0.8	1300	96.1	11.62	169,750	-50.4
1.0	1300	96.3	11.02	92,120	-52.7
1.2	1400	94.7	10.14	33,250	-37.1
1.6	1400	73.2	6.28	8,670	-40.1
2.0	1400	62.1	5.22	13,460	-18.1

then departed from linear relation as $x > 1.6$. Thus, the limit of $\text{Mg}_4(\text{Nb}_{2-x}\text{Sb}_x)\text{O}_9$ solid solutions is located at composition $x = 1.6$, in agreement with reference [8].

Figure 5 shows the surface micrographs of the as-sintered $\text{Mg}_4(\text{Nb}_{2-x}\text{Sb}_x)\text{O}_9$ ceramics for $x = 0, 0.8$, and 2.0 , respectively. As sintered at 1300°C , the homogeneously fine microstructures were revealed for $\text{Mg}_4\text{Nb}_2\text{O}_9$ ceramics [Fig. 5(a)]. The grain size of this composition is distributed around $0.6\text{--}1\ \mu\text{m}$. For the specimens with $x = 0.8$ and sintered at 1300°C , the dense microstructures without porosity shows the average grain size of about $3\ \mu\text{m}$ [Fig. 5(b)]. As for $x = 2.0$, the microstructures of $\text{Mg}_4\text{Sb}_2\text{O}_9$ ceramics shown in Fig. 5(c) are completely packed by plate-like grains isolated by pores. As the sintering temperature increased up to 1450°C , as shown in Fig. 5(d), the abnormal grain growth was observed for the $\text{Mg}_4(\text{Nb}_{1.2}\text{Sb}_{0.8})\text{O}_9$, which is in agreement with an obvious decrease of density shown in Fig. 1.

Figure 6 shows the dielectric constant, ϵ , and Qf value of $\text{Mg}_4(\text{Nb}_{2-x}\text{Sb}_x)\text{O}_9$ ($0 \leq x \leq 2$) ceramics as a function of the composition x for various sintering conditions. As shown in Fig. 6(a), the ϵ values of sintered ceramics decrease from 13.06 to 6.28 as x increases from 0 to 1.6. In Fig. 6(b), the Qf value of $\text{Mg}_4(\text{Nb}_{2-x}\text{Sb}_x)\text{O}_9$ ceramics is dependent on the compositions x and sintering temperatures. After sintering at 1300°C , the Qf values of $\text{Mg}_4(\text{Nb}_{2-x}\text{Sb}_x)\text{O}_9$ ceramics increase from 42,000 to 168,450 GHz as the composition x ranges from 0 to 0.4. The Qf values of $\text{Mg}_4(\text{Nb}_{2-x}\text{Sb}_x)\text{O}_9$ ceramics with $x = 0.4$ and 0.8 sintered at 1300°C are comparable to those of $\text{Mg}_4\text{Nb}_2\text{O}_9$ ceramics sintered at 1400°C .

However, for $x \geq 1.2$, Sb suppresses the Qf values due to the formation of plate-like grains, pores, abnormal grain growth, and impurity phases mentioned above.

The temperature coefficients of resonant frequency, τ_f of $\text{Mg}_4(\text{Nb}_{2-x}\text{Sb}_x)\text{O}_9$ ceramics sintered at appropriate temperatures are given in Table 1. As the composition x increases, the τ_f values increase. The τ_f values of all specimens have shown large negative values. The $\text{Mg}_4(\text{Nb}_{1.6}\text{Sb}_{0.4})\text{O}_9$ ceramics sintered at 1300°C for 5 h has the optimum microwave dielectric properties of $\epsilon = 12.26$, $\text{Qf} = 168\,450$ GHz (at 8.714 GHz), and $\tau_f = -56.4$ ppm/°C

4 Summary

The $\text{Mg}_4(\text{Nb}_{2-x}\text{Sb}_x)\text{O}_9$ ($0 \leq x \leq 2$) ceramics were prepared by a conventional solid reaction method. $\text{Mg}_4(\text{Nb}_{2-x}\text{Sb}_x)\text{O}_9$ solid solutions with composition x ranging from 0 to 1.6 had the ordered corundum structure of $\text{Mg}_4\text{Nb}_2\text{O}_9$. The lattice parameters, a , c and the volume V of $\text{Mg}_4(\text{Nb}_{2-x}\text{Sb}_x)\text{O}_9$ decreased with x as $x \leq 1.6$, whereas, the impurity phase $\text{Mg}_{11}\text{Sb}_4\text{O}_{21}$ appeared as the composition x ranged from 1.7 to 1.9. With a substitution of Sb^{5+} for Nb^{5+} ($0.4 \leq x \leq 0.8$), the sintering temperature of $\text{Mg}_4\text{Nb}_2\text{O}_9$ ceramics was reduced from 1400 to 1300°C without degenerating the Qf values, but the dielectric constant, ϵ , decreased from 13.06 to 6.28 as x varied from 0 to 1.6. Typically, the $\text{Mg}_4(\text{Nb}_{1.6}\text{Sb}_{0.4})\text{O}_9$ ceramics sintered at 1300°C for 5 h showed the optimum microwave dielectric properties: $\epsilon = 12.26$, $\text{Qf} = 168\,450$ GHz (at 8.714 GHz), $\tau_f = -56.4$ ppm/°C.

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